ICFP – Soft Matter

Einstein viscosity – Solution

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We mostly follow Ref. [1], in particular for the calculation of the flow. Another useful reference is Ref. [2].

1 Flow

1. We impose a shear flow at infinity: $u^{\infty}(x) = \dot{\gamma}y\hat{x}$. We use Stokes equations, hence everything (flow and motion of the sphere) should be linear in the imposed flow. We decompose $u^{\infty} = u_{\text{rot}}^{\infty} + u_{\text{strain}}^{\infty}$, where

$$\mathbf{u}_{\text{rot}}^{\infty}(\mathbf{x}) = \frac{\dot{\gamma}}{2}(y\hat{\mathbf{x}} - x\hat{\mathbf{y}})$$
 (1)

is a pure rotation, and

$$\boldsymbol{u}_{\mathrm{strain}}^{\infty}(\boldsymbol{x}) = \frac{\dot{\gamma}}{2}(y\hat{\boldsymbol{x}} + x\hat{\boldsymbol{y}})$$
 (2)

is a pure strain.

2. The rotation enforces a rotation of the sphere with the rate $-\dot{\gamma}/2$ around \hat{z} ; this flow is not disturbed. On the other hand

$$\boldsymbol{u}_{\text{strain}}^{\infty}(\boldsymbol{x}) = \frac{\dot{\gamma}}{2}(y\hat{\boldsymbol{x}} + x\hat{\boldsymbol{y}})$$
 (3)

is a pure strain. As the sphere is rigid, this flow must be disturbed to ensure the boundary condition u(|x|=a)=0.

3. We just have to study the disturbance created by the strain; we denote $u_{\text{strain}}^{\infty} = u^{\infty}$, and u the disturbance. We have

$$u_i^{\infty}(\boldsymbol{x}) = E_{ij}x_j,\tag{4}$$

with $E_{ii} = 0$, and the boundary condition is $u_i(r = a) = -E_{ij}x_j$, and $u_i(r \to \infty) \to 0$. The disturbance should satisfy the Stokes equations

$$\partial_i u_i = 0, \tag{5}$$

$$\mu \nabla^2 u_i = \partial_i p, \tag{6}$$

where p is the pressure and μ is the viscosity.

2 Solution for the flow

- **4.** Combining equations (5,6), we find $\partial_i \partial_i p = \mu \nabla^2 \partial_i u_i = 0$: p is harmonic.
- **5.** To compute the derivatives of 1/r, we use $\partial_i r = x_i/r$ and $\partial_i x_j = \delta_{ij}$. We get:

$$\partial_i \left(\frac{1}{r}\right) \propto \frac{x_i}{r^3},$$
 (7)

$$\partial_i \partial_j \left(\frac{1}{r}\right) \propto \frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5},$$
 (8)

$$\partial_i \partial_j \partial_k \left(\frac{1}{r} \right) \propto \frac{\delta_{ij} x_k + \delta_{ik} x_j + \delta_{jk} x_i}{r^5} - \frac{5 x_i x_j x_k}{r^7}.$$
 (9)

6. The only way to form a scalar with the tensor E_{ij} and these quantities is to have

$$p \propto E_{ij} \partial_i \partial_j \left(\frac{1}{r}\right) \propto E_{ij} \frac{x_i x_j}{r^5},$$
 (10)

where we have used that $E_{ii} = 0$. Hence

$$p = \lambda_1 E_{ij} \frac{x_i x_j}{r^5}. (11)$$

7. We then have to determine the flow u: it can be decomposed in a special solution to (6) and a harmonic part. The special solution can be written $u_i = x_i p/(2\mu)$, indeed:

$$\partial_j \partial_j (x_i p) = (\partial_j \partial_j x_i) p + 2(\partial_j x_i) (\partial_j p) + x_i \partial_j \partial_j p = 2\delta_{ij} \partial_j p = 2\partial_i p. \tag{12}$$

The harmonic solution has to be formed from the derivatives of 1/r above, leading to

$$u_{i} = \frac{\lambda_{1}}{2\mu} \frac{E_{jk} x_{i} x_{j} x_{k}}{r^{5}} + \lambda_{2} \frac{E_{ij} x_{j}}{r^{3}} + \lambda_{3} E_{jk} \left(\frac{\delta_{ij} x_{k} + \delta_{ik} x_{j} + \delta_{jk} x_{i}}{r^{5}} - \frac{5x_{i} x_{j} x_{k}}{r^{7}} \right). \tag{13}$$

8. In order to enforce incompressibility, we have to compute the divergence of the three terms. The divergence of the first term can be computed and is zero. The last term is $E_{ik}\partial_i\partial_j\partial_k(1/r)$ and since 1/r is harmonic the divergence of this term is zero. The divergence of the second term is not zero, which sets $\lambda_2 = 0$. The boundary condition $u_i(r=a) = -E_{ij}x_j$ leads to $\frac{\lambda_1}{2\mu a^5} = \frac{5\lambda_3}{a^7}$ and $2\lambda_3/a^5 = -1$, hence

$$p = -5\mu a^3 \frac{E_{ij} x_i x_j}{r^5},\tag{14}$$

$$u_i = -\frac{5}{2} \frac{a^3}{r^5} E_{jk} x_i x_j x_k \left(1 - \frac{a^2}{r^2} \right) - \frac{a^5}{r^5} E_{ij} x_j.$$
 (15)

3 Average stress in the fluid and viscosity

9. We have that $\partial_k(\sigma_{ik}x_j) = \sigma_{ij} + (\partial_k\sigma_{ik})x_j = \sigma_{ij}$, using that $\partial_k\sigma_{ik} = 0$. Hence, we can write

$$\bar{\sigma}_{ij} = \frac{1}{V} \int_{\mathcal{V}} \sigma_{ij} d\mathbf{x} = \frac{1}{V} \int_{\mathcal{V}} \partial_k (\sigma_{ik} x_j) d\mathbf{x} = \frac{1}{V} \int_{\partial \mathcal{V}} \sigma_{ik} x_j n_k d\mathbf{x}, \tag{16}$$

where n_k is a unit vector pointing towards the outside of the volume \mathcal{V} . This quantity is actually what is measured by a rheometer (which measures, for instance, the torque on the top plate).

10. Keeping only the dominant terms, we get

$$p = -5\mu a^3 \frac{E_{ij} x_i x_j}{r^5},\tag{17}$$

$$u_i = -\frac{5}{2} \frac{a^3}{r^5} E_{jk} x_i x_j x_k. \tag{18}$$

The stress disturbance is

$$\delta\sigma_{ij} = \mu(\partial_i u_j + \partial_j u_i) - p\delta_{ij} = 5\mu a^3 \left(-\frac{E_{ik} x_j x_k + E_{jk} x_i x_k}{r^5} + 5E_{kl} \frac{x_i x_j x_k x_l}{r^7} \right). \tag{19}$$

Integrating over the sphere of radius R, S_R , using that $n_i = x_i/R$, we get

$$\delta\bar{\sigma}_{ij} = \frac{5\mu a^3}{RV} \int_{\mathcal{S}_R} \left(-E_{ik} \frac{x_j x_k}{R^3} + 4E_{kl} \frac{x_i x_j x_k x_l}{R^5} \right) \tag{20}$$

$$= \frac{5\mu a^3}{V} \int_{\mathcal{S}_1} \left(-E_{ik} x_j x_k + 4E_{kl} x_i x_j x_k x_l \right) \tag{21}$$

$$= \frac{5\mu a^3}{V} \left[-E_{ik} \frac{4\pi}{3} \delta_{jk} + 4E_{kl} \frac{4\pi}{15} (\delta_{ij} \delta_{kl} + \delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) \right]$$
(22)

$$=\frac{4\pi\mu a^3}{V}E_{ij}. (23)$$

Note that this is the additionnal stress due to the disturbance u. The total average stress is

$$\bar{\sigma}_{ij} = 2\mu E_{ij} \left(1 + \frac{2\pi a^3}{V} \right) = 2\mu E_{ij} \left(1 + \frac{3v}{2V} \right), \tag{24}$$

where $v = (4/3)\pi a^3$ is the volume of a small sphere.

11. The average strain disturbance is

$$\delta \bar{e}_{ij} = \frac{1}{2V} \int_{\mathcal{V}} (\partial_i u_j + \partial_j u_i) \tag{25}$$

$$= \frac{1}{2VR} \int_{\mathcal{S}_R} (x_i u_j + x_j u_i) \tag{26}$$

$$= -\frac{5a^3}{2V} \int_{\mathcal{S}_1} E_{kl} x_i x_j x_k x_l \tag{27}$$

$$= -\frac{v}{V}E_{ij}. (28)$$

The average strain is thus

$$\bar{e}_{ij} = \left(1 - \frac{v}{V}\right) E_{ij}.\tag{29}$$

12. Summing the response over all the spheres and using the volume fraction ϕ , we get

$$\bar{\sigma}_{ij} = 2\mu E_{ij} \left(1 + \frac{3}{2} \phi \right), \tag{30}$$

$$\bar{e}_{ij} = (1 - \phi) E_{ij}.$$
 (31)

For small volume fraction, inverting the second equation gives $E_{ij} = (1 + \phi)\bar{e}_{ij}$ and

$$\bar{\sigma}_{ij} = 2\mu \bar{e}_{ij} \left(1 + \frac{5}{2} \phi \right) = 2\mu_E \bar{e}_{ij}, \tag{32}$$

where

$$\mu_E = \mu \left(1 + \frac{5}{2} \phi \right) \tag{33}$$

is the Einstein viscosity.

3.1 Alternative calculation of the viscosity

This is the calculation given in Ref. [1].

The average stress in the fluid is

$$\bar{\sigma}_{ij} = \frac{1}{V} \int_{\mathcal{V}} \sigma_{ij}(\boldsymbol{x}) d\boldsymbol{x} = 2\mu \bar{e}_{ij} - \bar{p}\delta_{ij} + \frac{1}{V} \int_{\mathcal{V}} \left[\sigma_{ij}(\boldsymbol{x}) - 2\mu e_{ij}(\boldsymbol{x}) + p(\boldsymbol{x})\delta_{ij} \right] d\boldsymbol{x}; \tag{34}$$

note that the integrand is non zero over the particles only. The last term in the integrand and \bar{p} should vanish by symmetry. Noting that $\sigma_{ij} = \partial_k(\sigma_{ik}x_j)$, we can transform the integral in a surface integral

$$\bar{\sigma}_{ij} = 2\mu E_{ij} + \frac{1}{V} \int_{\mathcal{S}_R} \left[\sigma_{ik} x_j n_k - \mu (n_i u_j + n_j u_i) \right] d\mathbf{x}, \tag{35}$$

where the integral is performed over the sphere of radius R. Choosing $R \to \infty$, we just have to care about the dominant component of the flow,

$$u_i^{\text{dom}} = -\frac{5}{2} \frac{a^3}{r^5} E_{jk} x_i x_j x_k, \tag{36}$$

it is associated to a strain rate

$$e_{ij}^{\text{dom}} = -\frac{5a^3}{2} \left[\frac{E_{kl} x_k x_l}{r^5} \left(\delta_{ij} - \frac{5x_i x_j}{r^2} \right) + \frac{E_{ik} x_j x_k + E_{jk} x_i x_k}{r^5} \right]. \tag{37}$$

With the stress $\sigma_{ij}^{\rm dom} = 2\mu e_{ij}^{\rm dom} - p\delta_{ij}$, the surface integral reads (using the surface integrals given in App. A)

$$\int_{S_R} \left[\sigma_{ik} x_j n_k - \mu (n_i u_j + n_j u_i) \right] d\mathbf{x} = \frac{20\pi}{3} \mu a^3 E_{ij}.$$
 (38)

Summing over the N particles in the suspension, and using the volume fraction $\phi = \frac{4\pi a^3 N}{3V}$, we get

$$\bar{\sigma}_{ij} = 2\mu \left(1 + \frac{5}{2}\phi \right) E_{ij},\tag{39}$$

where the Einstein viscosity appears:

$$\mu_E = \mu \left(1 + \frac{5}{2} \phi \right). \tag{40}$$

A Surface integrals of polynomials

Using spherical coordinates, we can compute the following integrals over the unit sphere:

$$\int_{\mathcal{S}} x_i x_j \mathrm{d}\boldsymbol{x} = \frac{4\pi}{3} \delta_{ij},\tag{41}$$

$$\int_{S} x_i x_j x_k x_l d\mathbf{x} = \frac{4\pi}{15} \left(\delta_{ij} \delta_{kl} + \delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk} \right). \tag{42}$$

References

- [1] Élisabeth Guazzelli, Jeffrey F. Morris, and Sylvie Pic. A Physical Introduction to Suspension Dynamics. Cambridge Texts in Applied Mathematics. Cambridge University Press, 2011.
- [2] L. D. Landau and E. M. Lifshitz. *Fluid Mechanics, Second Edition: Volume 6.* Course of theoretical physics / by L. D. Landau and E. M. Lifshitz, Vol. 6. Butterworth-Heinemann, 2 edition, jan 1987.